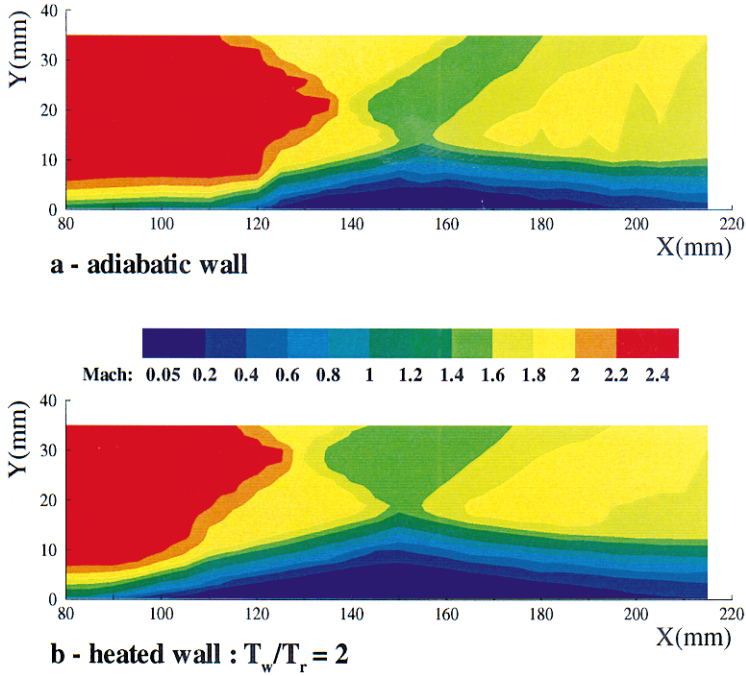


FIGURE 8.3.31 Wall temperature effect on an oblique shock reflection at $M_\infty = 2.4$ (Délery, 1992).

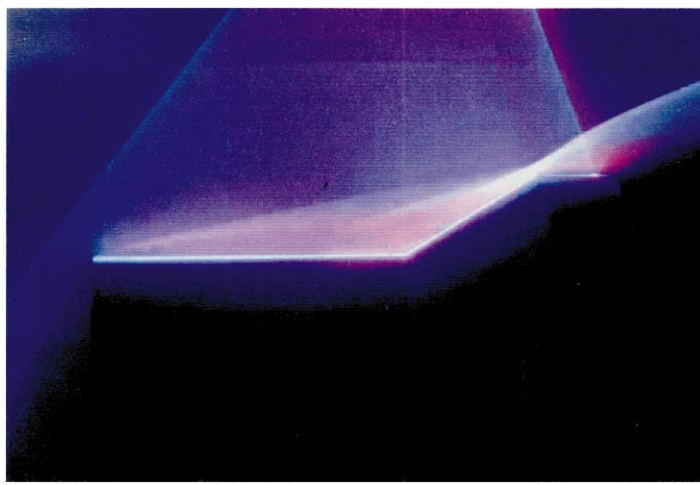


FIGURE 8.3.35 The hollow cylinder-flare model for assessment of code accuracy on a laminar high Mach number interaction (Chanetz *ete al.*, 1998).

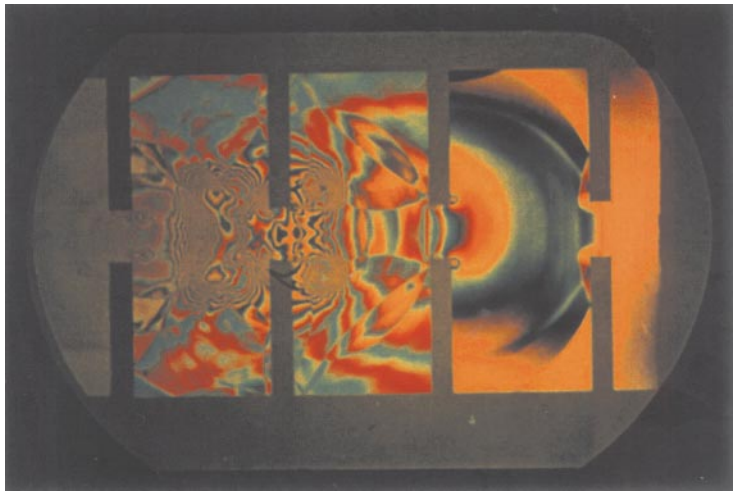


FIGURE 10.9 The process shown in Fig. 10.8 at a later time instant; now it is shown as an interferogram.

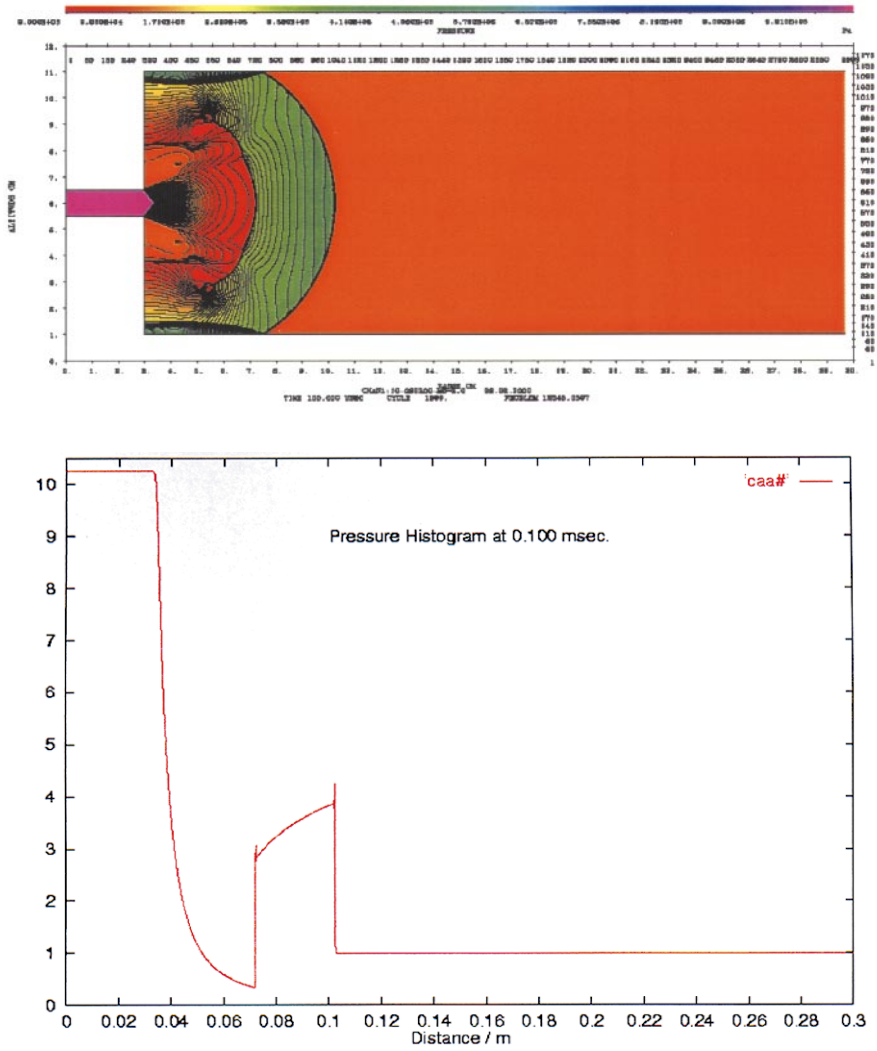
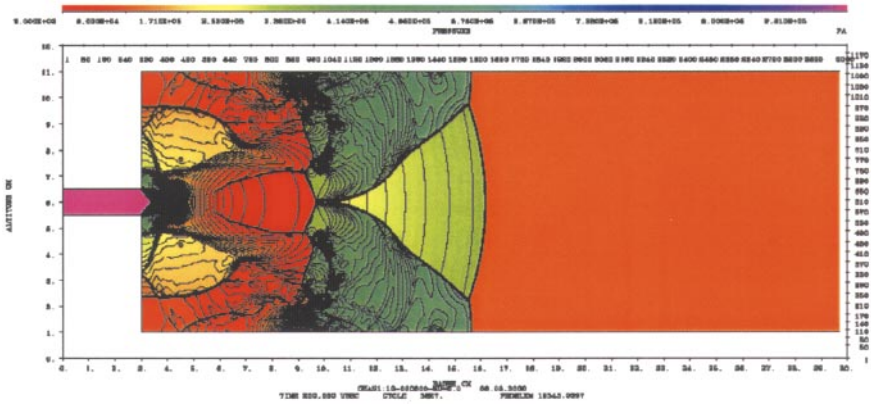


FIGURE 10.42 SHAMRC's isobars and pressure histograms (along the plane of symmetry: $y = 6\,\text{cm}$) for the propagation of the transmitted shock wave ($M_0 = 3.0$) through an abrupt channel enlargement. The area ratio is 1 : 10. The figure shows the state of the flow (a) 100 μsec, (b) 200 μsec, and (c) 400 μsec after flow initiation. The shock position at initiation time ($t = 0\,\mu\text{sec}$) is $x = 2.5\,\text{cm}$.



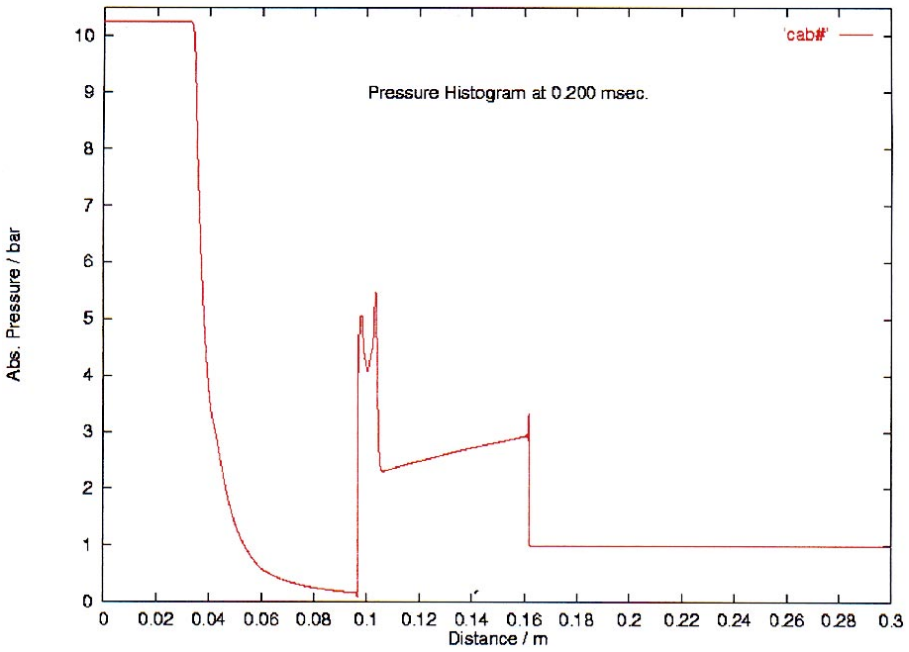
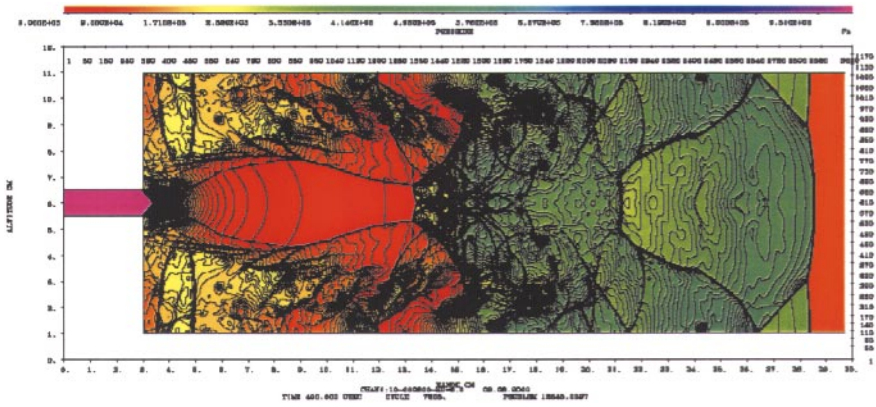


FIGURE 10.42 (*continued*)



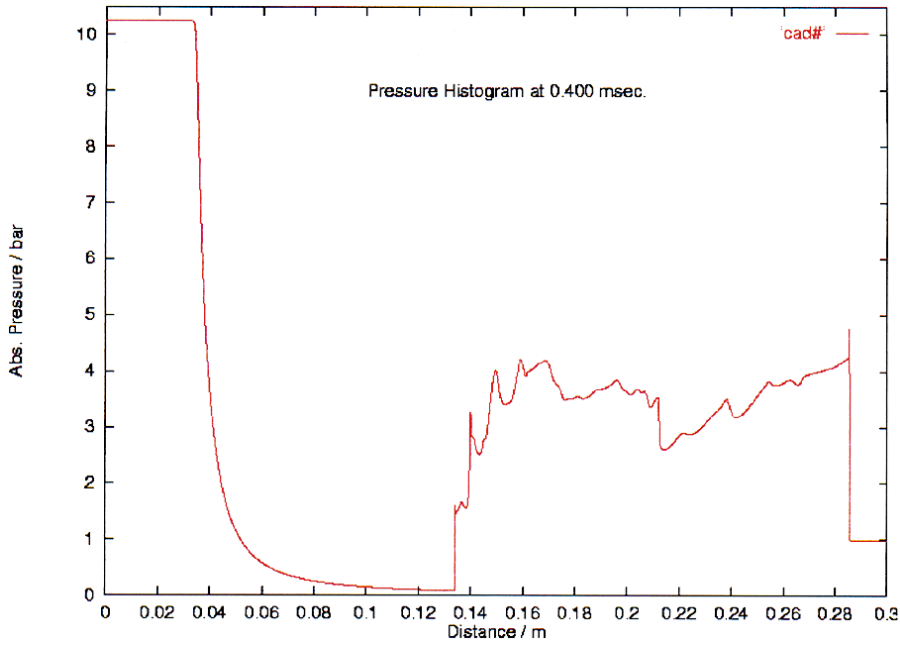


FIGURE 10.42 (*continued*)

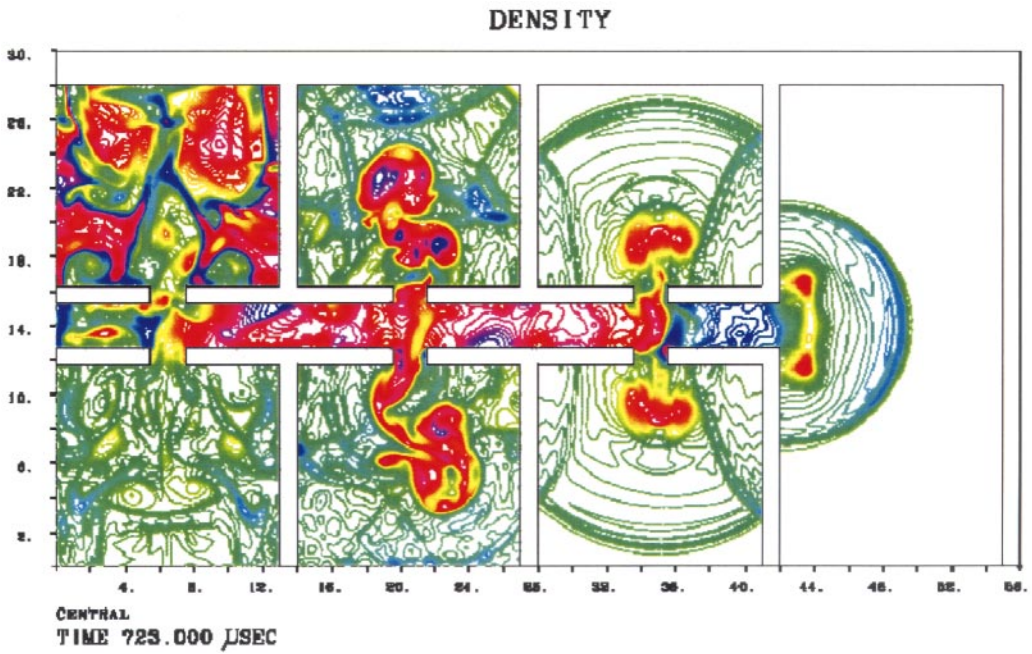


FIGURE 10.44 Isopycnics resulting from the propagation of a detonation wave (blast wave) in a multichamber system (2D). Rooms with a door are connected through a corridor. The wave is "numerically" initiated using a built-in option of SHAMRC by specifying a certain amount of a selectable explosive.