

# The Displacement Sheet and Hydrostatics

Chapter 4 introduced the concepts of:

- Bonjean curves
- a displacement sheet as a concise way of calculating the displacement of a body defined by a table of offsets,
- hydrostatic curves.

Rather than place a lot of related numerical work in the main text, an example of how they can be derived is placed in this appendix.

Table B.1 is a displacement sheet, using Microsoft Excel, for a vessel in which the waterplanes are 2 m apart and the sections 14.1 m apart. The actual half ordinates defining the underwater form of a body are shown in bold. For greater definition in way of the turn of bilge, an intermediate waterplane has been introduced between waterplanes 5 and 6, the Simpson's multipliers being adjusted accordingly. To simplify the arithmetic the appendages which would usually be found below number 6, waterplane and aft of ordinate 11 have been ignored.

The figures in Row 6 are obtained from multiplying the half ordinates in Row 5 by the corresponding Simpson's multipliers in Row 3. Thus cell M6 is the product of the contents of cells M3 and M5. Cell R6 is the sum of the cells in Row 6 and represents the area of the section at ordinate 1 up to the summer waterline (SWL). The figures in Column S are the result of multiplying the figures in Column R by the Simpson's multipliers in Column B. Cell S28 is the sum of the figures in Column S and represents the volume of the immersed body. The figures in Column U are the products of Columns S and T. Cell U28 is the sum of the figures in Column U and represents the moment of the buoyancy force about amidships.

Correspondingly, the figure in cell D7 is the product of the figure in cell C7 and the Simpson's multiplier in cell B7. Then cell D28 is the sum of the figures in Column D and represents the area of waterplane 6. The figures in Row 30 are the result of multiplying the figures in Row 28 by the Simpson's multipliers in Row 3, noting that the SM for column D is that appearing in Column C, and so on. Cell R30 is the sum of the figures in Row 30 and

**TABLE B.1 Displacement Sheet**

A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	R	S	T	U
1	Waterline	6		5.5	5	3	2								SWL				
2																			
3	Ordinate	SM	0.5	2	1.5	4	2	4	1							$F(A)$	$F(A) \times$ SM	Lever aft	$F(M)$
4																			
5	1	0.000	0.000	0.000	0.000	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100			
6	0.000	0.000	0.000	0.000	0.400	0.200	0.400	0.100	1.100	1.1	-5								
7	2	0.500	2.000	1.060	4.240	1.640	6.560	2.760	11.040	3.640	14.560	4.440	17.760	5.200	20.800				
8	0.250	2.120	2.460	11.040	7.280	17.760	5.200	46.110	184.44	-4	-737.76								
9	3	1.900	3.800	3.280	6.560	4.700	9.400	6.660	13.320	8.100	16.200	9.100	18.200	9.840	19.680				
10	0.950	6.560	7.050	26.640	16.200	36.400	9.840	103.640	207.28	-3	-621.84								
11	4	4.500	18.000	6.800	27.200	8.600	34.400	10.640	42.560	11.800	47.200	12.480	49.920	12.800	51.200				
12	2.250	13.600	12.900	42.560	23.600	49.920	12.800	157.630	630.52	-2	-1261.04								
13	5	2	7.240	14.480	10.100	20.200	11.800	23.600	13.300	26.600	13.800	27.600	14.000	28.000	14.040	28.080			

14	3.620	20.200	17.700	53.200	27.600	56.000	14.040	192.360	384.72	-1	-384.72					
15	6	4	9,000	36,000	11,900	47,600	13,240	52,960	14,200	56,800	14,500	58,000	14,400	14,400	57,600	
16	4,500	23,800	19,860	56,800	29,000	58,000	14,400	206.360	825.44	0	0					
17	7	2	7,900	15,800	10,700	21,400	12,400	24,800	13,640	27,280	14,080	28,160	14,220	28,440	14,200	28,400
18	3,950	21,400	18,600	54,560	28,160	56,880	14,200	197.750	395.5	1	395.5					
19	8	4	5,500	22,000	8,000	32,000	9,700	38,800	11,900	47,600	13,020	52,080	13,540	54,160	13,700	54,800
20	2,750	16,000	14,550	47,600	26,040	54,160	13,700	174.800	699.2	2	1398.4					
21	9	2	3,000	6,000	4,500	9,000	6,040	12,080	8,640	17,280	10,700	21,400	12,020	24,040	12,600	25,200
22	1,500	9,000	9,060	34,560	21,400	48,080	12,600	136.200	272.4	3	817.2					
23	10	4	0,940	3,760	1,560	6,240	2,160	8,640	3,700	14,800	5,700	22,800	8,000	32,000	10,060	40,240
24	0,470	3,120	3,240	14,800	11,400	32,000	10,060	75.090	300.36	4	1201.44					
25	11	1	0,100	0,100	0,100	0,100	0,100	0,100	0,100	0,100	0,100	0,100	0,100	0,100	0,100	0,100
26	0,050	0,200	0,150	0,400	0,200	0,400	0,300	2,700	2,7	5	13.5					
27																
28	121,940	174,540	211,340	257,480	288,200	310,720	327,400	3903.66	815.18							

(Continued)





compares the vertical centre of buoyancy (VCB) position by taking moments about the SWL and the keel. It will be noted that the two figures added together correspond very closely to the draught of 10 m.

## Waterplane and Section Areas

Embedded in Table B.1 are figures that can be used to derive the area of each waterplane and the area of each section up to the SWL. The former are in the second column of figures under each waterline (Columns D, F, H, etc.); the latter in the second row against each ordinate (Rows 6, 8, 10, etc.). These could be calculated within the main table, but for clarity of presentation they are here presented in Table B.3. The tonnes per centimetre immersion are calculated for each waterplane.

Tables can be produced for each waterplane, similar to Table 3.2 in Chapter 3, to give the area, centroid position and the longitudinal and transverse moments of inertia. These are presented in Tables B.4–B.10.

*Note:* In the row against  $I(\text{long})$ , the first figure is the moment of inertia about amidships and the second is the inertia about the centre of flotation.

For the body up to 3WL and 5WL, part-displacement sheets can be constructed as given in Tables B.11 and B.12, respectively.

A convenient way of calculating the volume of displacement and VCB position for waterlines 2 and 4 (as well as the SWL) is to plot the waterplane areas to obtain the figures for intermediate waterplanes as given in Table B.13.

## Bonjean Curves

The Bonjean curves can be calculated, for any section, by integration up to each waterline in turn. The Simpson's rule chosen in each case, and hence the multiplying factor to be used, will depend upon the number of ordinates. Table B.14 derives the section areas up to 5.5WL and between SWL and 2WL using Simpson's 5, 8, 1 rule. Table B.15 derives the section areas between the SWL and 4WL and 5WL using the 1, 3, 3, 1 rule and between SWL and 5WL using the 1, 4, -1 rule. Then a table of cross-sectional areas can be drawn up as given in Table B.16 from which the Bonjean curves can be drawn. Figure B.1 uses the data given in Table B.16 to show the Bonjean curves for ordinates 2, 3, 4 and 5.

## Volumes and Longitudinal Centres of Buoyancy

The section areas can be used to calculate the volumes of displacement up to each waterline and the corresponding longitudinal centres of buoyancy (LCBs) as given in Table B.17.

**TABLE B.3 Waterplane and Section Areas**

<b>Waterplane Areas</b>										
Waterplane	6	5.5	5	4	3	2	SWL			
$F(A)$	121.94	174.54	211.34	257.48	288.20	310.72	327.40			
Area = $F(A) \times 2$ (14.1/3)	1146.24	1640.68	1986.60	2420.31	2709.08	2920.77	3077.56			
TPC (tonnes/CM) = area(1.025/100)	11.75	16.82	20.36	24.81	27.77	29.94	31.54			
<b>Section areas up to SWL</b>										
Ordinate	1	2	3	4	5	6	7	8	9	10 11
$F(A)$	1.10	46.11	103.64	157.63	192.36	206.36	197.75	174.80	136.20	75.09 2.70
Area up to SWL = $F(A) \times 2 \times (2/3)$	1.47	61.48	138.19	210.17	256.48	275.15	263.67	233.07	181.60	100.12 3.60

**TABLE B.4 SWL**

Station	Half Ord, y	SM	F(A)	Lever	F(M)	Lever	F(l) long	yyy	F(l) trans
1	0.10	1	0.10	5	0.50	5	2.50	0	0
2	5.20	4	20.80	4	83.20	4	332.80	141	562
3	9.84	2	19.68	3	59.04	3	177.12	953	1906
4	12.80	4	51.20	2	102.40	2	204.80	2097	8389
5	14.04	2	28.08	1	28.08	1	28.08	2768	5535
6	14.40	4	57.60	0	0.00	0	0.00	2986	11,944
7	14.20	2	28.40	-1	-28.40	-1	28.40	2863	5727
8	13.70	4	54.80	-2	-109.60	-2	219.20	2571	10,285
9	12.60	2	25.20	-3	-75.60	-3	226.80	2000	4001
10	10.06	4	40.24	-4	-160.96	-4	643.84	1018	4072
11	1.30	1	1.30	-5	-6.50	-5	32.50	2	2
Total			327.40		-107.84		1896.04		52,423
Area = $(2/3) \times 14.1 \times F(A) =$									
3077.56									
Moment									
-14,293.1									
Centre of flotation (CF)									
-4.6443									
f(long)									
3,543,346									
f(trans)									
16,4258.9									



**TABLE B.5 2WL**

Station	Half Ord, y	SM	F(A)	Lever	F(M)	Lever	F(0) long	yyy	F(0) trans
1	0.10	1	0.10	5	0.50	5	2.50	0	0
2	4.44	4	17.76	4	71.04	4	284.16	88	350
3	9.10	2	18.20	3	54.60	3	163.80	754	1507
4	12.48	4	49.92	2	99.84	2	199.68	1944	7775
5	14.00	2	28.00	1	28.00	1	28.00	2744	5488
6	14.50	4	58.00	0	0.00	0	0.00	3049	12,195
7	14.22	2	28.44	-1	-28.44	-1	28.44	2875	5751
8	13.54	4	54.16	-2	-108.32	-2	216.64	2482	9929
9	12.02	2	24.04	-3	-72.12	-3	216.36	1737	3473
10	8.00	4	32.00	-4	-128.00	-4	512.00	512	2048
11	0.10	1	0.10	-5	-0.50	-5	2.50	0	0
Total			310.72		-83.40		1654.08		48,516
Area = (2/3) × 14.1 × F(A) =		2920.768							
Moment		-11,053.8							
CF		-3.78456							
I(long)		3,091,168							
I(trans)		152,017.3							

**TABLE B.6 3WL**

Station	Half Ord, y	SM	F(A)	Lever	F(M)	Lever	F(l) long	yyy	F(l) trans
1	0.10	1	0.10	5	0.50	5	2.50	0	0
2	3.64	4	14.56	4	58.24	4	232.96	48	193
3	8.10	2	16.20	3	48.60	3	145.80	531	1063
4	11.80	4	47.20	2	94.40	2	188.80	1643	6572
5	13.80	2	27.60	1	27.60	1	27.60	2628	5256
6	14.50	4	58.00	0	0.00	0	0.00	3049	12,195
7	14.08	2	28.16	-1	-28.16	-1	28.16	2791	5583
8	13.02	4	52.08	-2	-104.16	-2	208.32	2207	8829
9	10.70	2	21.40	-3	-64.20	-3	192.60	1225	2450
10	5.70	4	22.80	-4	-91.20	-4	364.80	185	741
11	0.10	1	0.10	-5	-0.50	-5	2.50	0	0
Total			288.20		-58.88		1394.04		42,881
Area = $(2/3) \times 14.1 \times F(A) =$									
Moment					2709.08				
CF					-7803.96				
					-2.88067				
f(long)					2,605,201				2,582,721
f(trans)					134,359.4				

**TABLE B.7 4WL**

Station	Half Ord, y	SM	F(A)	Lever	F(M)	Lever	F(l)long	yyy	F(l) trans
1	0.10	1	0.10	5	0.50	5	2.50	0	0
2	2.76	4	11.04	4	44.16	4	176.64	21	84
3	6.66	2	13.32	3	39.96	3	119.88	295	591
4	10.64	4	42.56	2	85.12	2	170.24	1205	4818
5	13.30	2	26.60	1	26.60	1	26.60	2353	4705
6	14.20	4	56.80	0	0.00	0	0.00	2863	11,453
7	13.64	2	27.28	-1	-27.28	-1	27.28	2538	5075
8	11.90	4	47.60	-2	-95.20	-2	190.40	1685	6741
9	8.64	2	17.28	-3	-51.84	-3	155.52	645	1290
10	3.70	4	14.80	-4	-59.20	-4	236.80	51	203
11	0.10	1	0.10	-5	-0.50	-5	2.50	0	0
Total			257.48		-37.68		1108.36		34,960
Area = (2/3) × 14.1 × F(A) = 2420.312									
Moment = -4994.11									
CF = -2.06341									
I(long) = 2,071,319									
I(trans) = 109,541.9									

**TABLE B.8 5WL**

Station	Half Ord, y	SM	F(A)	Lever	F(M)	Lever	F(l) long	yyy	F(l) trans
1	0.00	1	0.00	5	0.00	5	0.00	0	0
2	1.64	4	6.56	4	26.24	4	104.96	4	18
3	4.70	2	9.40	3	28.20	3	84.60	104	208
4	8.60	4	34.40	2	68.80	2	137.60	636	2544
5	11.80	2	23.60	1	23.60	1	23.60	1643	3286
6	13.24	4	52.96	0	0.00	0	0.00	2321	9284
7	12.40	2	24.80	-1	-24.80	-1	24.80	1907	3813
8	9.70	4	38.80	-2	-77.60	-2	155.20	913	3651
9	6.04	2	12.08	-3	-36.24	-3	108.72	220	441
10	2.16	4	8.64	-4	-34.56	-4	138.24	10	40
11	0.10	1	0.10	-5	-0.50	-5	2.50	0	0
Total			211.34		-26.86		780.22		23,284
Area = $(2/3) \times 14.1 \times F(A) =$									
1986.596									
Moment									
-3560.02									
CF									
-1.79202									
f(long)									
1,458,086									
f(trans)									
72,957.44									

**TABLE B.9 5.5WL**

Station	Half Ord, y	SM	F(A)	Lever	F(M)	Lever	F(0) long	yyy	F(0) trans
1	0.00	1	0.00	5	0.00	5	0.00	0	0
2	1.06	4	4.24	4	16.96	4	67.84	1	5
3	3.28	2	6.56	3	19.68	3	59.04	35	71
4	6.80	4	27.20	2	54.40	2	108.80	314	1258
5	10.10	2	20.20	1	20.20	1	20.20	1030	2061
6	11.90	4	47.60	0	0.00	0	0.00	1685	6741
7	10.70	2	21.40	-1	-21.40	-1	21.40	1225	2450
8	8.00	4	32.00	-2	-64.00	-2	128.00	512	2048
9	4.50	2	9.00	-3	-27.00	-3	81.00	91	182
10	1.56	4	6.24	-4	-24.96	-4	99.84	4	15
11	0.10	1	0.10	-5	-0.50	-5	2.50	0	0
Total			174.54		-26.62		588.62		14,830
Area = $(2/3) \times 14.1 \times F(A) =$ 1640.676									
Moment = -3528.21									
CF = -2.15046									
$I(\text{long}) = 1,100,021$ 1,092,434									
$I(\text{trans}) = 46,466.79$									

**TABLE B.10 6WL**

Station	Half Ord, y	SM	F(A)	Lever	F(M)	Lever	F(l) long	YY	F(l) trans
1	0.00	1	0.00	5	0.00	5	0.00	0	0
2	0.50	4	2.00	4	8.00	4	32.00	0	1
3	1.90	2	3.80	3	11.40	3	34.20	7	14
4	4.50	4	18.00	2	36.00	2	72.00	91	365
5	7.24	2	14.48	1	14.48	1	14.48	380	759
6	9.00	4	36.00	0	0.00	0	0.00	729	2916
7	7.90	2	15.80	-1	-15.80	-1	15.80	493	986
8	5.50	4	22.00	-2	-44.00	-2	88.00	166	666
9	3.00	2	6.00	-3	-18.00	-3	54.00	27	54
10	0.94	4	3.76	-4	-15.04	-4	60.16	1	3
11	0.10	1	0.10	-5	-0.50	-5	2.50	0	0
Total			121.94		-23.46		373.14		5763
Area = $(2/3) \times 14.1 \times F(A) =$									
1146.236									
Moment									
-3109.39									
CF									
-2.71269									
f(long)									
697,329.3									
688,894.4									
f(trans)									
18,056.23									

**TABLE B.11 Part-Displacement Sheet up to 3WL**

Waterline	6	5.5	5	4	3							
Ordinate	SM	0.5	2	1.5	4	1	F(A)	F(A) × SM	Lever aft	F(M)	Area	CB aft
1	1	<b>0.000</b>	0.000	<b>0.000</b>	0.000	<b>0.100</b>	0.100	<b>0.100</b>	0.100	0.100	0.100	
		0.000	0.000	0.000	0.400	0.100	0.500	0.5	-5	-2.5	0.67	
2	4	<b>0.500</b>	2.000	<b>1.060</b>	4.240	<b>1.640</b>	6.560	<b>2.760</b>	11.040	<b>3.640</b>	14.560	
		0.250	2.120	2.460	11.040	3.640	19,510	78.04	-4	-312.16	26.01	
3	2	<b>1.900</b>	3.800	<b>3.280</b>	6.560	<b>4.700</b>	9.400	<b>6.660</b>	13.320	<b>8.100</b>	16.200	
		0.950	6.560	7.050	26.640	8.100	49,300	98.6	-3	-295.8	65.73	
4	4	<b>4.500</b>	18.000	<b>6.800</b>	27.200	<b>8.600</b>	34.400	<b>10.640</b>	42.560	<b>11.800</b>	47.200	
		2.250	13.600	12.900	42.560	11.800	83,110	332.44	-2	-664.88	110.81	
5	2	<b>7.240</b>	14.480	<b>10.100</b>	20.200	<b>11.800</b>	23.600	<b>13.300</b>	26.600	<b>13.800</b>	27.600	
		3.620	20.200	17.700	53.200	13.800	108,520	217.04	-1	-217.04	144.69	
6	4	<b>9.000</b>	36.000	<b>11.900</b>	47.600	<b>13.240</b>	52.960	<b>14.200</b>	56.800	<b>14.500</b>	58.000	
		4.500	23.800	19.860	56.800	14.500	119,460	477.84	0	0	159.28	
7	2	<b>7.900</b>	15.800	<b>10.700</b>	21.400	<b>12.400</b>	24.800	<b>13.640</b>	27.280	<b>14.080</b>	28.160	
		3.950	21.400	18.600	54.560	14.080	112,590	225.18	1	225.18	150.12	

(Continued)





**TABLE B.12** Part-Displacement Sheet up to 5WL

Waterline	6	5.5	5	0.5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Ordinate	SM	0.5	2	0.5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1	1	<b>0.000</b>	0.000	<b>0.000</b>	0.000	<b>0.000</b>	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2	4	<b>0.500</b>	2.000	<b>1.060</b>	4.240	<b>1.640</b>	6.560	0.820	3.190	12.76	-4	-51.04	4.25		
3	2	<b>1.900</b>	3.800	<b>3.280</b>	6.560	<b>4.700</b>	9.400	2.350	9.860	19.72	-3	-59.16	13.15		
4	4	<b>4.500</b>	18.000	<b>6.800</b>	27.200	<b>8.600</b>	34.400	4.300	20.150	80.60	-2	-161.20	26.87		
5	2	<b>7.240</b>	14.480	<b>10.100</b>	20.200	<b>11.800</b>	23.600	5.900	29.720	59.44	-1	-59.44	39.63		
6	4	<b>9.000</b>	36.000	<b>11.900</b>	47.600	<b>13.240</b>	52.960	6.620	34.920	139.68	0	0.00	46.56		
7	2	<b>7.900</b>	15.800	<b>10.700</b>	21.400	<b>12.400</b>	24.800	6.200	31.550	63.10	1	63.10	42.07		

(Continued)

**TABLE B.12 Part-Displacement Sheet up to 5WL—(cont.)**

Waterline	6		5.5		5		F(A)	F(A) X SM	Lever aft	F(M)	Area	CB aft
	SM	0.5	2	0.5	0.5	0.5						
8	4	<b>5.500</b>	22.000	<b>8.000</b>	32.000	<b>9.700</b>	38.800					
		2.750	16.000		4.850		23.600	94.40	2	188.80	31.47	
9	2	<b>3.000</b>	6.000	<b>4.500</b>	9.000	<b>6.040</b>	12.080					
		1.500	9.000		3.020		13.520	27.04	3	81.12	18.03	
10	4	<b>0.940</b>	3.760	<b>1.560</b>	6.240	<b>2.160</b>	8.640					
		0.470	3.120		1.080		4.670	18.68	4	74.72	6.23	
11	1	<b>0.100</b>	0.100	<b>0.100</b>	0.100	<b>0.100</b>	0.100					
		0.050	0.200		0.050		0.300	0.30	5	1.50	0.40	
		121.940		174.540		211.340		515.72		78.40	2.143	
		60.97	349.08		105.67	515.72						
Lever		0	0.5		1							
Moment		0	174.54		105.67	280.21						
CB above base										1.087		

**TABLE B.13** Volumes and VCBs for intermediate waterplanes

Waterline	Area	SM	F(V)	Lever	F(M)1	Lever	F(M)2	SM	F(V)	Lever	F(M)	SM	F(V)	Lever	F(M)
SWL	3078	1	3078	0	0	10	30,780								
1.5	3015	4	12,060	1	12,060	9	108,540								
2	2921	2	5842	2	11,684	8	46,736	1	2921	8	23,368				
2.5	2820	4	11,280	3	33,840	7	78,960	4	11,280	7	78,960				
3	2709	2	5418	4	21,672	6	32,508	2	5418	6	32,508	1	2709	6	16,254
3.5	2570	4	10,280	5	51,400	5	51,400	4	10,280	5	51,400	4	10,280	5	51,400
4	2420	2	4840	6	29,040	4	19,360	2	4840	4	19,360	2	4840	4	19,360
4.5	2230	4	8920	7	62,440	3	26,760	4	8920	3	26,760	4	8920	3	26,760
5	1987	2	3974	8	31,792	2	7948	2	3974	2	7948	2	3974	2	7948
5.5	1641	4	6564	9	59,076	1	6564	4	6564	1	6564	4	6564	1	6564
6	1146	1	1146	10	11,460	0	0	1	1146	0	0	1	1146	0	0
Volume			24,467.33						18,447.67						12,811
CB below SWL					4.42037										
CB above keel							5.57963				4.460691				3.337913

**TABLE B.14** Calculations for Bonjean Curves

Ordinate	Area Between Keel and 5.5WL			Areas Between SWL and 2WL			F(A)	F(V)	Area	F(A)	Area	F(V)
	SM	5	8	-1	8	5						
1	0.000	0.000	0.000	<b>0.000</b>	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100
	0.000	0.000	0.000	0.000	0.00	0.00	0.00	-0.100	0.800	0.500	1.20	0.40
2	<b>0.500</b>	2.000	<b>1.060</b>	4.240	<b>1.640</b>	<b>3.640</b>	14.560	<b>4.440</b>	17.760	<b>5.200</b>	20.800	20.800
	2.500	8.480	-1.640	9.34	1.56	6.23	-3.640	35.520	26.000	57.88	19.29	77.17333
3	<b>1.900</b>	3.800	<b>3.280</b>	6.560	<b>4.700</b>	<b>8.100</b>	16.200	<b>9.100</b>	18.200	<b>9.840</b>	19.680	19.680
	9.500	26.240	-4.700	31.04	5.17	10.35	-8.100	72.800	49.200	113.90	37.97	75.93333
4	<b>4.500</b>	18.000	<b>6.800</b>	27.200	<b>8.600</b>	<b>11.800</b>	47.200	<b>12.480</b>	49.920	<b>12.800</b>	51.200	51.200
	22.500	54.400	-8.600	68.30	11.38	45.53	-11.800	99.840	64.000	152.04	50.68	202.72
5	<b>7.240</b>	14.480	<b>10.100</b>	20.200	<b>11.800</b>	<b>13.800</b>	27.600	<b>14.000</b>	28.000	<b>14.040</b>	28.080	28.080
	36.200	80.800	-11.800	105.20	17.53	35.07	-13.800	112.000	70.200	168.40	56.13	112.2667
6	<b>9.000</b>	36.000	<b>11.900</b>	47.600	<b>13.240</b>	<b>14.500</b>	58.000	<b>14.500</b>	58.000	<b>14.400</b>	57.600	57.600
	45.000	95.200	-13.240	126.96	21.16	84.64	-14.500	116.000	72.000	173.50	57.83	231.3333

7	2	7.900	15.800	10.700	21.400	12.400	14.080	28.160	14.220	28.440	14.200	28.400	
		39.500	85.600	-12.400	112.70	18.78	37.57	-14.080	113.760	71.000	170.68	56.89	113.7867
8	4	5.500	22.000	8.000	32.000	9.700	13.020	52.080	13.540	54.160	13.700	54.800	
		27.500	64.000	-9.700	81.80	13.63	54.53	-13.020	108.320	68.500	163.80	54.60	218.4
9	2	3.000	6.000	4.500	9.000	6.040	10.700	21.400	12.020	24.040	12.600	25.200	
		15.000	36.000	-6.040	44.96	7.49	14.99	-10.700	96.160	63.000	148.46	49.49	98.97333
10	4	0.940	3.760	1.560	6.240	2.160	5.700	22.800	8.000	32.000	10.060	40.240	
		4.700	12.480	-2.160	15.02	2.50	10.01	-5.700	64.000	50.300	108.60	36.20	144.8
11	1	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	1.300	1.300	
		0.500	0.800	-0.100	1.20	0.20	0.20	-0.100	0.800	6.500	7.20	2.40	2.4
		FV)			299.11						1278.187		
		Volume			1405.83						6007.48		

**TABLE B.15 Section Areas Between SWL and 4WL and 5WL**

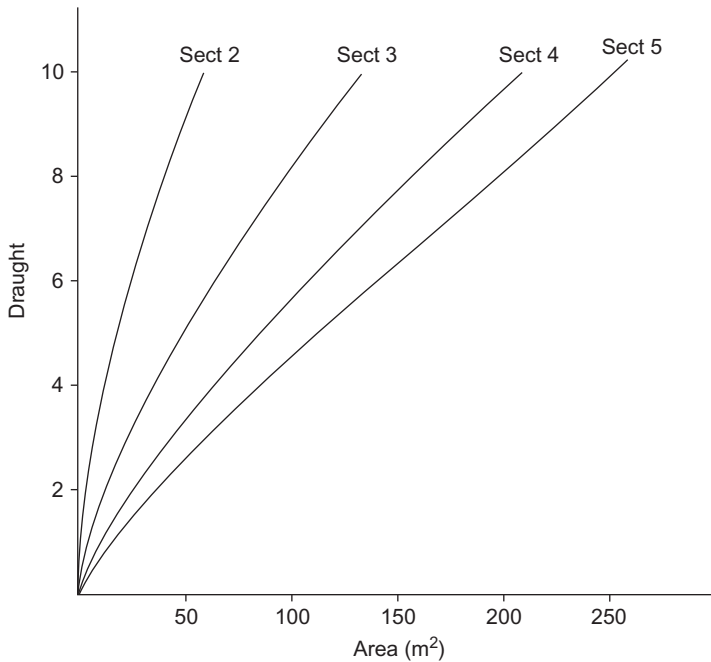
WL	SM	1	4	3	2	SWL	F(A)				
Ordinate	SM	1	3	3	1	(4WL)	Area(4)				
1	1	<b>0.00</b>	0.00	<b>0.10</b>	0.10	<b>0.10</b>	<b>0.10</b>	0.10			
		0.00	0.40	0.20	0.40	0.10	1.10	1.47			
		0.10	0.10	0.30	0.30	0.10	0.80	1.20			
2	4	<b>1.64</b>	6.56	<b>2.76</b>	11.04	<b>3.64</b>	14.56	<b>4.44</b>	17.76	<b>5.20</b>	20.80
		1.64	11.04	7.28	17.76	5.20	42.92	57.23			
		2.76	10.92	13.32	5.20	32.20	48.30				
3	2	<b>4.70</b>	9.40	<b>6.66</b>	13.32	<b>8.10</b>	16.20	<b>9.10</b>	18.20	<b>9.84</b>	19.68
		4.70	26.64	16.20	36.40	9.84	93.78	125.04			
		6.66	24.30	27.30	68.10						
4	4	<b>8.60</b>	34.40	<b>10.64</b>	42.56	<b>11.80</b>	47.20	<b>12.48</b>	49.92	<b>12.80</b>	51.20
		8.60	42.56	23.60	49.92	12.80	137.48	183.31			
		10.64	35.40	37.44	96.28						
5	2	<b>11.80</b>	23.60	<b>13.30</b>	26.60	<b>13.80</b>	27.60	<b>14.00</b>	28.00	<b>14.04</b>	28.08
		11.80	53.20	27.60	56.00	14.04	162.64	216.85			
		13.30	41.40	42.00	110.74						

6	4	<b>13.24</b>	52.96	<b>14.20</b>	56.80	<b>14.50</b>	58.00	<b>14.50</b>	58.00	<b>14.40</b>	57.60	14.40	171.44	228.59
		13.24		56.80		29.00	58.00		58.00		14.40			
				14.20		43.50	43.50	1.0	14.40		115.60			173.40
7	2	<b>12.40</b>	24.80	<b>13.64</b>	27.28	<b>14.08</b>	28.16	<b>14.22</b>	28.44	<b>14.20</b>	28.40			
		12.40		54.56		28.16	56.88		14.20		166.20			221.60
				13.64		42.24	42.66		14.20		112.74			169.11
8	4	<b>9.70</b>	38.80	<b>11.90</b>	47.60	<b>13.02</b>	52.08	<b>13.54</b>	54.16	<b>13.70</b>	54.80			
		9.70		47.60		26.04	54.16		13.70		151.20			201.60
				11.90		39.06	40.62		13.70		105.28			157.92
9	2	<b>6.04</b>	12.08	<b>8.64</b>	17.28	<b>10.70</b>	21.40	<b>12.02</b>	24.04	<b>12.60</b>	25.20			
		6.04		34.56		21.40	48.08		12.60		122.68			163.57
				8.64		32.10	36.06		12.60		89.40			134.10
10	4	<b>2.16</b>	8.64	<b>3.70</b>	14.80	<b>5.70</b>	22.80	<b>8.00</b>	32.00	<b>10.06</b>	40.24			
		2.16		14.80		11.40	32.00		10.06		70.42			93.89
				3.70		17.10	24.00		10.06		54.86			82.29
11	1	<b>0.10</b>	0.10	<b>0.10</b>	0.10	<b>0.10</b>	0.10	<b>0.10</b>	0.10	<b>0.10</b>	1.30			
		0.10		0.40		0.20	0.40		1.30		2.40			3.20
				0.10		0.30	0.30		0.10		2.00			3.00

Area to 5WL = F(A)(5WL) × 2 × 2/3 = (4/3)F(A)(5WL).  
Area to 4WL = F(A)(4WL) × 2 × 2 × (3/8) = 1.5F(A)(4WL).

**TABLE B.16** Table of Section Areas

<i>Ord</i>	Area to						
	6WL	5.5WL	5WL	4WL	3WL	2WL	SWL
1	0.00	0.00	0.00	0.27	0.67	1.07	1.47
2	0.00	1.56	4.25	13.18	26.01	42.19	61.48
3	0.00	5.17	13.15	36.04	65.73	100.22	138.19
4	0.00	11.38	26.87	65.75	110.81	159.49	210.17
5	0.00	17.53	39.63	90.37	144.69	200.35	256.48
6	0.00	21.16	46.56	101.75	159.28	217.32	275.15
7	0.00	18.78	42.07	94.56	150.12	206.78	263.67
8	0.00	13.63	31.47	75.15	125.23	178.47	233.07
9	0.00	7.49	18.03	47.50	86.43	132.11	181.60
10	0.00	2.50	6.23	17.83	36.44	63.92	100.12
11	0.00	0.20	0.40	0.60	1.20	1.60	3.60

**FIGURE B.1** Bonjean curves.



**TABLE B.17** Volumes and LCBs

Ord	SM	Lever	Area to						
			5.5WL			5WL			
			Area	F(V)	F(M)	Area	F(V)	F(M)	
1	1	5	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	4	4	1.56	6.24	24.96	4.25	17.00	68.00	
3	2	3	5.17	10.34	31.02	13.15	26.30	78.90	
4	4	2	11.38	45.52	91.04	26.87	107.48	214.96	
5	2	1	17.53	35.06	35.06	39.63	79.26	79.26	
6	4	0	21.16	84.64	0.00	46.56	186.24	0.00	
7	2	-1	18.78	37.56	-37.56	42.07	84.14	-84.14	
8	4	-2	13.63	54.52	-109.04	31.47	125.88	-251.76	
9	2	-3	7.49	14.98	-44.94	17.53	35.06	-105.18	
10	4	-4	2.50	10.00	-40.00	6.23	24.92	-99.68	
11	1	-5	0.20	0.20	-1.00	0.40	0.40	-2.00	
Total			99.40	299.06	-50.46	686.68	-101.64		
Volume	CB aft		1405.582	-2.379074		3227.396	-2.087033		
Displacement			1440.722			3308.081			

(Continued)

**TABLE B.17 Volumes and LCBs—(cont.)**

Ord	SM	Lever	4WL			3WL		
			Area	F(N)	F(M)	Area	F(N)	F(M)
1	1	5	0.27	0.27	1.35	0.67	0.67	3.35
2	4	4	13.18	52.72	210.88	26.01	104.04	416.16
3	2	3	36.04	72.08	216.24	65.73	131.46	394.38
4	4	2	65.75	263.00	526.00	110.81	443.24	886.48
5	2	1	90.37	180.74	180.74	144.69	289.38	289.38
6	4	0	101.75	407.00	0.00	159.28	637.12	0.00
7	2	-1	94.56	189.12	-189.12	150.12	300.24	-300.24
8	4	-2	75.15	300.60	-601.20	125.23	500.92	-1001.84
9	2	-3	47.50	95.00	-285.00	86.43	172.86	-518.58
10	4	-4	17.83	71.32	-285.28	36.44	145.76	-583.04
11	1	-5	0.60	0.60	-3.00	1.20	1.20	-6.00
Total				1632.45	-228.39		2726.89	-419.95
Volume	CB aft			7672.515	-1.972678		12,816.38	-2.171446
Displacement				7864.328			13,136.79	

Ord	SM	Lever	2WL			SWL		
			Area	F(V)	F(M)	Area	F(V)	F(M)
1	1	5	1.07	1.07	5.35	1.47	1.47	7.35
2	4	4	42.19	168.76	675.04	61.48	245.92	983.68
3	2	3	100.22	200.44	601.32	138.19	276.38	829.14
4	4	2	159.49	637.96	1275.92	210.17	840.68	1681.36
5	2	1	200.35	400.70	400.70	256.48	512.96	512.96
6	4	0	217.32	869.28	0.00	275.15	1100.60	0.00
7	2	-1	206.78	413.56	-413.56	263.67	527.34	-527.34
8	4	-2	178.47	713.88	-1427.76	233.07	932.28	-1864.56
9	2	-3	132.11	264.22	-792.66	181.60	363.20	-1089.60
10	4	-4	63.92	255.68	-1022.72	100.12	400.48	-1601.92
11	1	-5	1.60	1.60	-8.00	3.60	3.60	-18.00
Total				3927.15	-706.37		5204.91	-1086.93
Volume	CB aft			18,457.61	-2.536144		24,463.08	-2.944472
Displacement				18,919.05			25,074.65	

**TABLE B.18 KB and KM Values**

WL	6	5.5	5	4	3	2	SWL
Trans I	18,056	46,467	72,957	109,542	134,359	152,017	164,259
Volume, V	0	1406	3232	7505	12,816	18,470	24,463
Trans BM		33.05	22.57	14.60	10.48	8.23	6.71
KB	0	0.53	1.09	2.22	3.34	4.46	5.58
Trans KM		33.58	23.66	16.82	13.82	12.69	12.29
Long I	688,900	1,092,400	1,451,700	2,061,000	258,700	3,049,300	3,477,000
Long BM		777	449	275	202	165	142
Long KM		777	450	277	205	170	148
<i>Additional data for plotting hydrostatic curves</i>							
Mass displacement	0	1441	3313	7693	13,136	18,932	25,075
TPC	11.75	16.82	20.36	24.81	27.77	29.94	31.54
CF aft	2.71	2.15	1.79	2.06	2.88	3.78	4.64
LCB aft		2.38	2.09	1.97	2.17	2.54	2.94
<i>Further if KG = 11 m</i>							
Long GM		766	439	266	194	159	137
MCT		7830	10,320	14,510	18,070	21,350	24,360

## Metacentric Diagram

As discussed in Chapter 4, the metacentric diagram shows how the VCB and metacentre positions vary with draught. The VCB values have been found above. BM is given by  $I/V$  and values are derived in Table B.18 using  $I$  and  $V$  figures from the other tables. KM is  $KB + BM$  and thus a metacentric diagram can be produced for the body which is the subject of this appendix. Table B.18 also includes a calculation of the longitudinal metacentre position which is needed to obtain the hydrostatic curves. The metacentric diagram is plotted in Figure B.2.

## Hydrostatic Curves

Chapter 4 also introduced the concept of hydrostatic curves. The information in Table B.18, assuming a KG of 11 m, is used to plot Figure B.3.

*Note:* The data used in the Bonjean and hydrostatic curves can be derived in a number of different ways. Those above have been selected to give the reader an idea of the procedures involved.

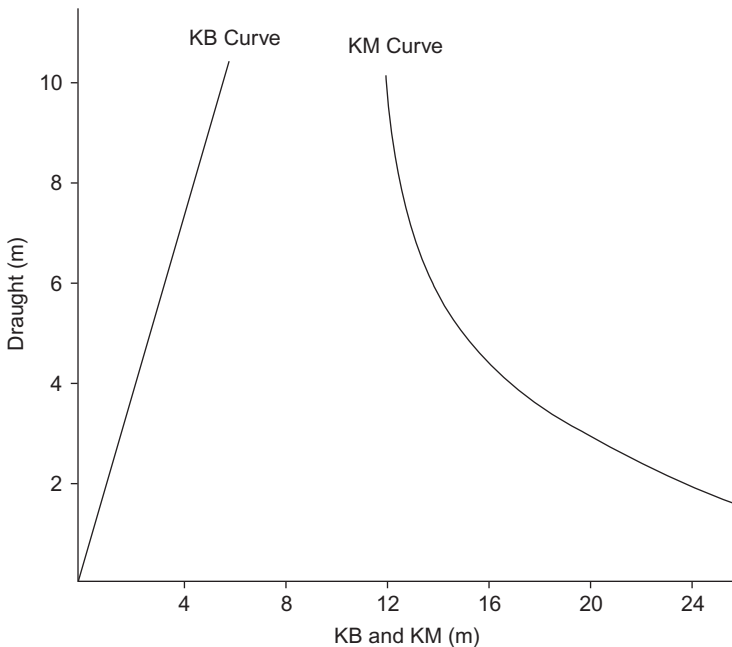


FIGURE B.2 Metacentric diagram.

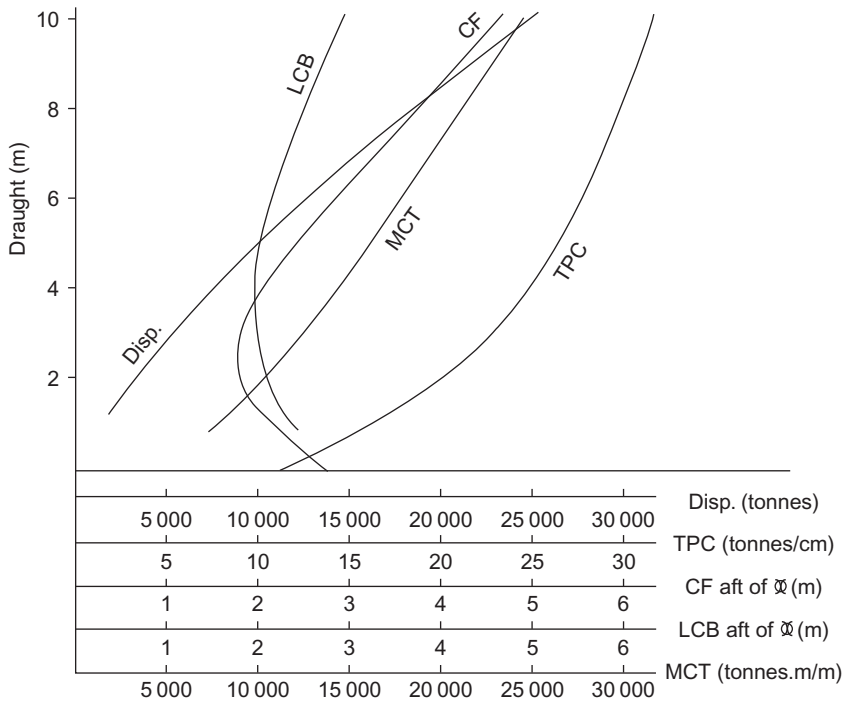


FIGURE B.3 Hydrostatic curves.